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of 4 copies, series A, and the following attachments.**General Mills, Inc.**

MECHANICAL DIVISION
Engineering Research and Development Department
 2003 East Hennepin Avenue
 Minneapolis 13, Minnesota

Direct Line: MAin 7481

1 October 1954

Dear Bud:

I am sending you under separate cover five (5) copies of the 263P Technical Report, PERSONNEL-CARRYING BALLOONS

At this time, I also want to clarify the status of the plastic valves. Since we have designated the current model, the M3 Plastic Valve, it would probably simplify matters by applying the M1 designation to the original plastic valve, and so on. In any case, here is the status of the valves up to the present.

<u>Valve</u>	<u>Capacity</u>	<u>Tested</u>	<u>Production</u>
M1	13#	2-54, 5-54	Yes
M2	40#	7-54	No
M3	60#	No	Yes (present contract)

Very truly yours,

GENERAL MILLS, INC.
 Engineering Research
 and Development

J. C. Warren
 J. C. WARREN
 Balloon and Meteorological
 Systems Group

JCW:jw

25X1

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R2-459

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JUN 19, 1978

General Mills, Inc.
Mechanical Division

ENGINEERING RESEARCH & DEVELOPMENT
DEPARTMENT

2003 EAST HENNEPIN AVENUE
MINNEAPOLIS 13, MINN.

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This document consists of 5 pages and is number 1
of 13 copies, series A, and the following attachments.
*Appendix
of Photor*

263P TECHNICAL REPORT

Contract No. Nonr 875(00)
Annex IV

PREPARED FOR
THE OFFICE OF NAVAL RESEARCH
WASHINGTON, D. C.

Prepared by: J. C. Warren

Date: 30 September 1954

Report No. 1332

GENERAL MILLS, INC.
Mechanical Division
ENGINEERING RESEARCH AND DEVELOPMENT
2003 E. Hennepin Ave.
Minneapolis 13, Minn.

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APPENDIX

Time/Altitude Flight 1140

Trajectory Flight 1140

Gross Load vs. Altitude 263P

263P Drawings

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SUMMARY

A personnel-carrying balloon with a volume of 8000 cubic feet was designed according to "Natural Shape" specifications. The design was subjected to a hangar test on 17 February 1954 and was flown successfully on 6 May 1954. This report will cover both experiments.

I. INTRODUCTION

A study of the sphere cone envelopes previously used resulted in the finding of both horizontal and vertical stress concentrations in the envelopes. In the "Natural Shape" balloon, circumferential stresses are eliminated. This concept motivated the redesign of personnel-carrying balloons.

II. THE NEW DESIGNA. Theory of the Natural Shape

Since balloons can be manufactured in any desired shape of closed surface, it is clear that there is a most desired shape.

The principal consideration was stresses, the consequent strain and the relationship between surface area and volume contained. Stresses on the surface area arise from (1) supporting the payload and (2) gas pressure. Those stresses which have a direction which is tangent to the surface and which lie in a vertical plane are called meridional stresses. Tests have shown that the meridional stresses are transferred from the tapes onto the surface area uniformly.

Curvature in a stresses surface produces an inward force per unit area. In a balloon, this force is opposed by the difference in pressure of gas inside and outside. If the inward force created by the meridional stress is nullified everywhere by the gas pressure, the balloon is said to have a "Natural Shape" and has zero circumferential tension.

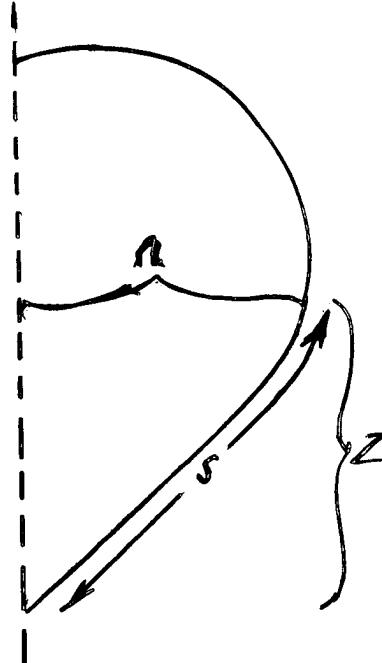
These ideas were conceived and reduced to practice by General Mills, Inc. under Air Force sponsorship in 1951. Since then, much of the work done on balloon design has been implemented by the University of Minnesota Balloon Physics Group development of design nomographs from use of the analog computer.

Each shape is characterized by a value of the "balloon fabric parameter Ξ ", where Ξ is a dimensionless parameter that enters the differential equations when the effect of finite fabric weight is taken into account. The method of obtaining the shapes from the differential equations is as follows:

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Nine different values of Σ were chosen, and for each value the differential equations were solved using the analog computer. These nine shapes were then normalized to give the shape coordinates T, Z, S for balloons of unit gore length, where r and Z give the profile of the balloon and S is the distance of a point on the profile from the bottom apex (measured up along the gore).



Since the Σ value is a ratio of the gross load to balloon weight, the design becomes unique for each case. The following design is based on a maximum load and provides ample material for the envelope to assume its natural shape.

B. Selection of Proper Shape

1. Each shape is characterized by a value of Σ , where $\Sigma = 0$ corresponds to the so-called "weightless natural shape", and larger corresponding to the more oblate shape with heavier fabric weight. The proper value of Σ is uniquely determined by the following quantities.

V = Volume

L = Payload suspended from bottom apex.

W = Weight of fabric material per unit area.

$$= .344 \frac{W}{L} \left[1 + \frac{W}{L} \right]^{3/2}$$

$$= .028$$

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Using the University of Minnesota nomograph, curve #2 was selected where $\Sigma = .05$. This Σ value produces an envelope profile as shown in Figure

Note: The nine different values of Σ chosen were from zero to .40 in .05 increments. Since the optimum value (.028) lies between curve for 0 and .05, .05 was selected. This means there is slightly more material than needed for the envelope to assume its natural shape with existing loads.

2. Tailoring of the shape selection consisted of the following.

a. The gore layout was modified at stations #19 and #29 so that the profile would be symmetrical.

b. To provide for a two point suspension at the bottom apex of the balloon, two gores were tailored in the following manner. A line was drawn from a point, corresponding to the desired width at the base of the balloon, tangent to the gore. The resulting pattern provided the necessary width at the balloon base and precluded the inclusion of separate wedge gores. This device in no way affected the balloon diameter, and the minimum addition had only a negligible effect on the volume of the balloon.

III. THE HANGAR TEST

1. Objectives

A balloon was fabricated on the basis of the foregoing specifications and hangar-tested on 17 February 1954. Objectives of the test were as follows:

- a. Test the new design.
- b. Determine effects of tailored gores to provide a two point suspension.
- c. Measure M₁ plastic value capacity in a stable atmosphere.
- d. Confirm the design volume.

2. Details of Testing

The following pictures show the balloon at 200 pounds of lift, 400 pounds of lift and when full at 517 pounds of lift.

At full inflation the system was lifted off the ground and thrown down again several times sending shock waves up and down the fabric and creating a whipping action.

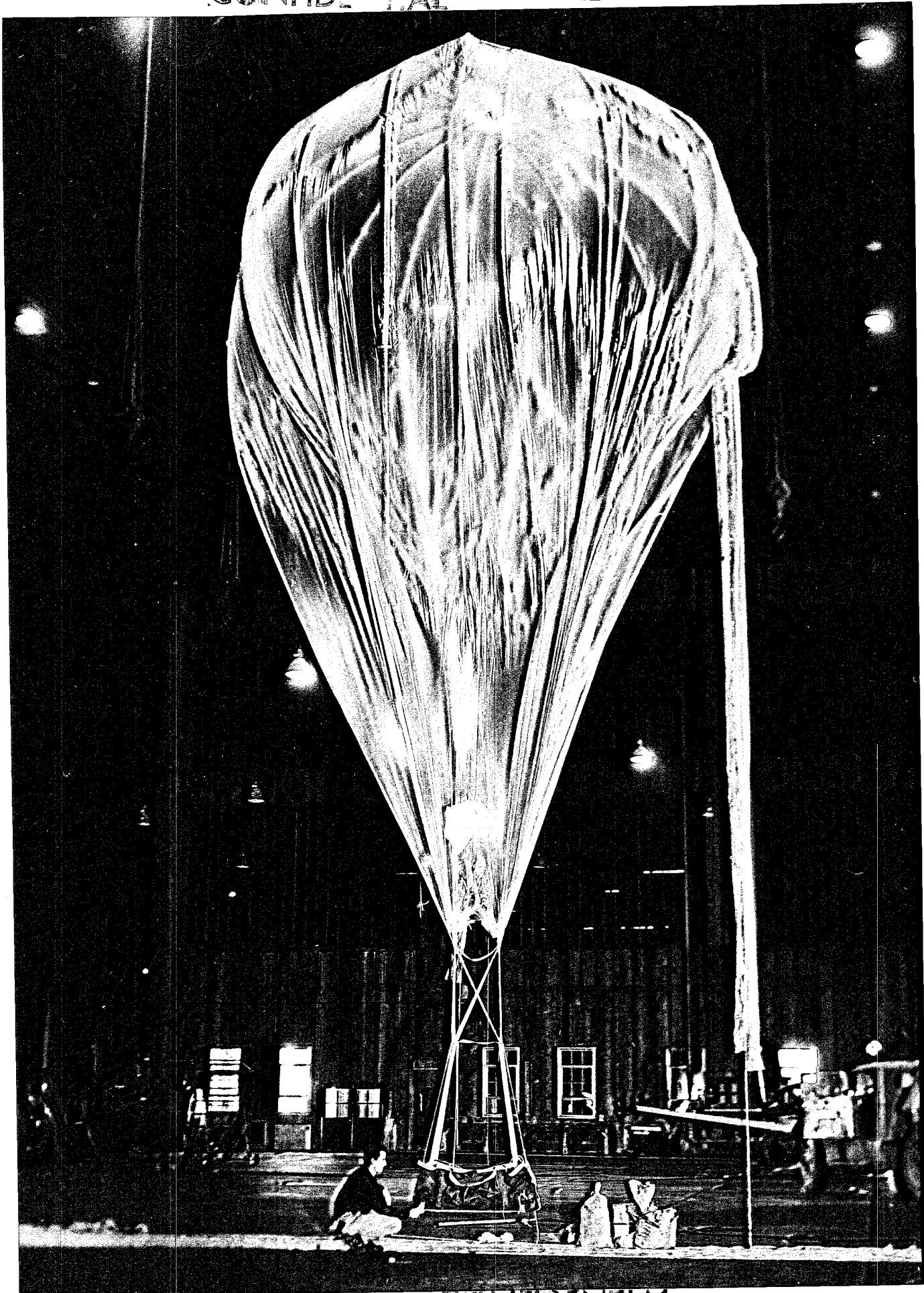
Two tests of the value, one for one minute and the other for five minutes, were made.

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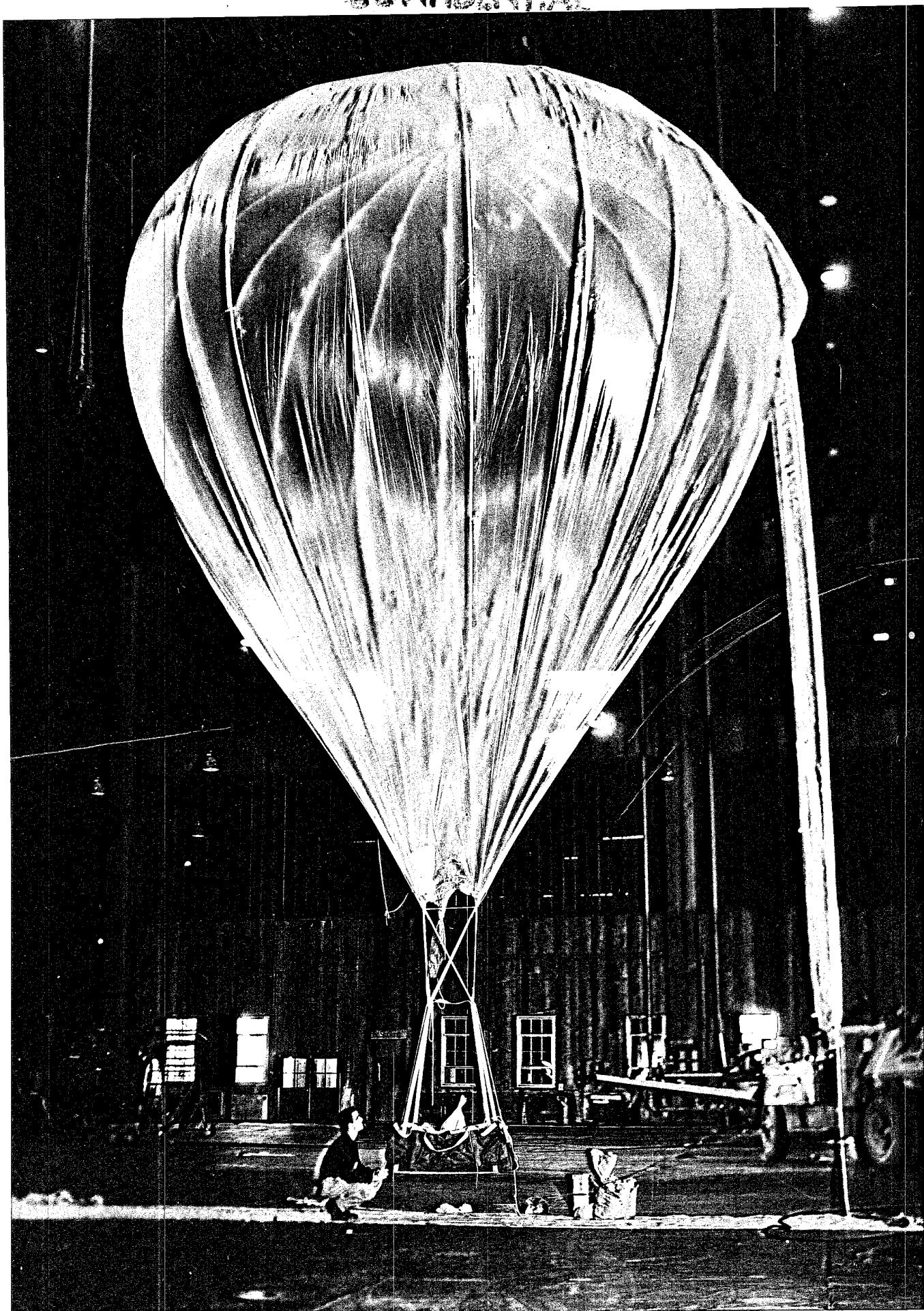
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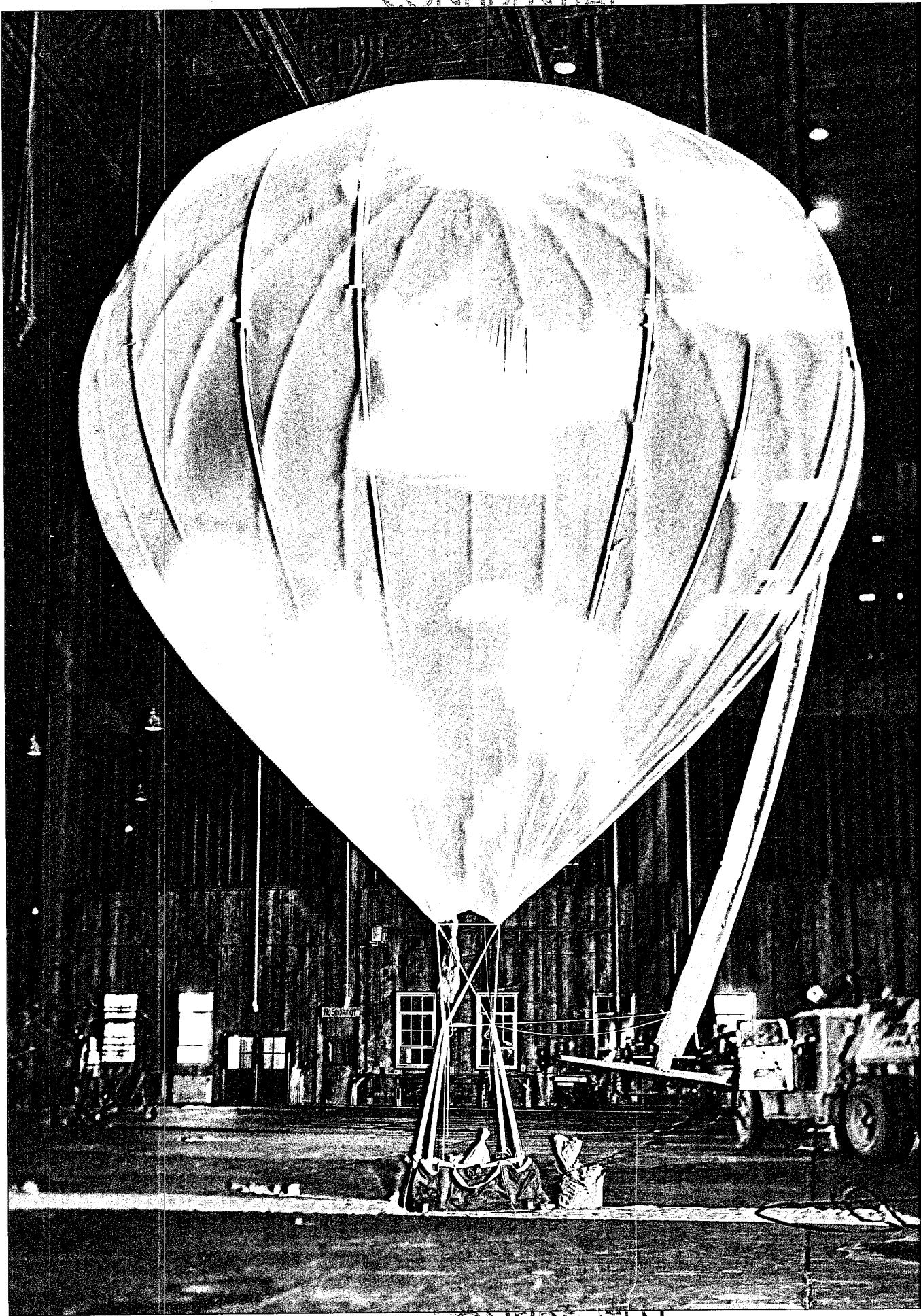
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- 4 -

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3. Conclusions and Recommendations

- a. Generally, the new design proved very efficient, remaining undamaged under conditions more severe than those expected in flight.
- b. It was decided to apply tapes to the wedge gore. This will provide symmetry to load-bearing members on the balloon.
- c. The M1 plastic value loss of lift in pounds per minute was consistent in both testing periods at 14 lbs./min.
- d. The gross load of 517 pounds, using helium as the lifting gas, confirmed the design volume at 7900 cubic feet.

IV. THE FLIGHT TEST

1. Objectives

A manned balloon flight, GMI #1140, was made on 6 May 1954. Objectives of the flight were as follows:

- a. To flight-test the new 263P balloon.
- b. To determine the flight capabilities of the 263P balloon.
- c. To approve the 263P balloon for production.
- d. To test the hydreneal generator.

2. Details of Testing

The inflation and launching was accomplished without any real difficulty except that it was not possible to meet the time schedule because of difficulties with the hydreneal generator. Surface winds remained less than 5 MPH during most of the period which simplified handling the balloon over the three and one-half hour inflation period.

Take-off was made at 0750 with the balloon rising at 400 F.P.M. to its ceiling of 5000 feet. The flight was characterized by the instability that was evidenced shortly after the balloon had reached its ceiling. The pilot was kept busy riding out the series of up and down drafts. A total ballast of 29 pounds was required to keep the system in a safe altitude range. Total valving time for the four hour duration was only 1 1/4 minutes with the major portion of this being required for landing. Indicative of the instability was the pilot's notation at 1130. "Small brown leaf observed in air near balloon - altitude 3200 feet". The first attempt at a landing resulted in the balloon being caught in a downdraft over a wooded area. The balloon descended into tree tops approximately 10 feet above the base of the balloon. Numerous tears in the balloon were observed. The balloon then rose above the tree and was valved to landing a few minutes later.

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3. Conclusions and Recommendations

- a. The 263P balloon withstood a severe test flight and performed excellently under existing conditions.
- b. The 263P, as designed, is an acceptable item and ready for production.
- c. The hydroneal generator did not produce the 4000 CFH as indicated but gave 3000 CFH, prolonging inflation over 1 1/2 hours.
- d. That the hydroneal gas has a distinct ammonia odor was evidenced by the pilot in flight and the crew members during inflation.

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APPENDIX





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FILE COPY THE SEC

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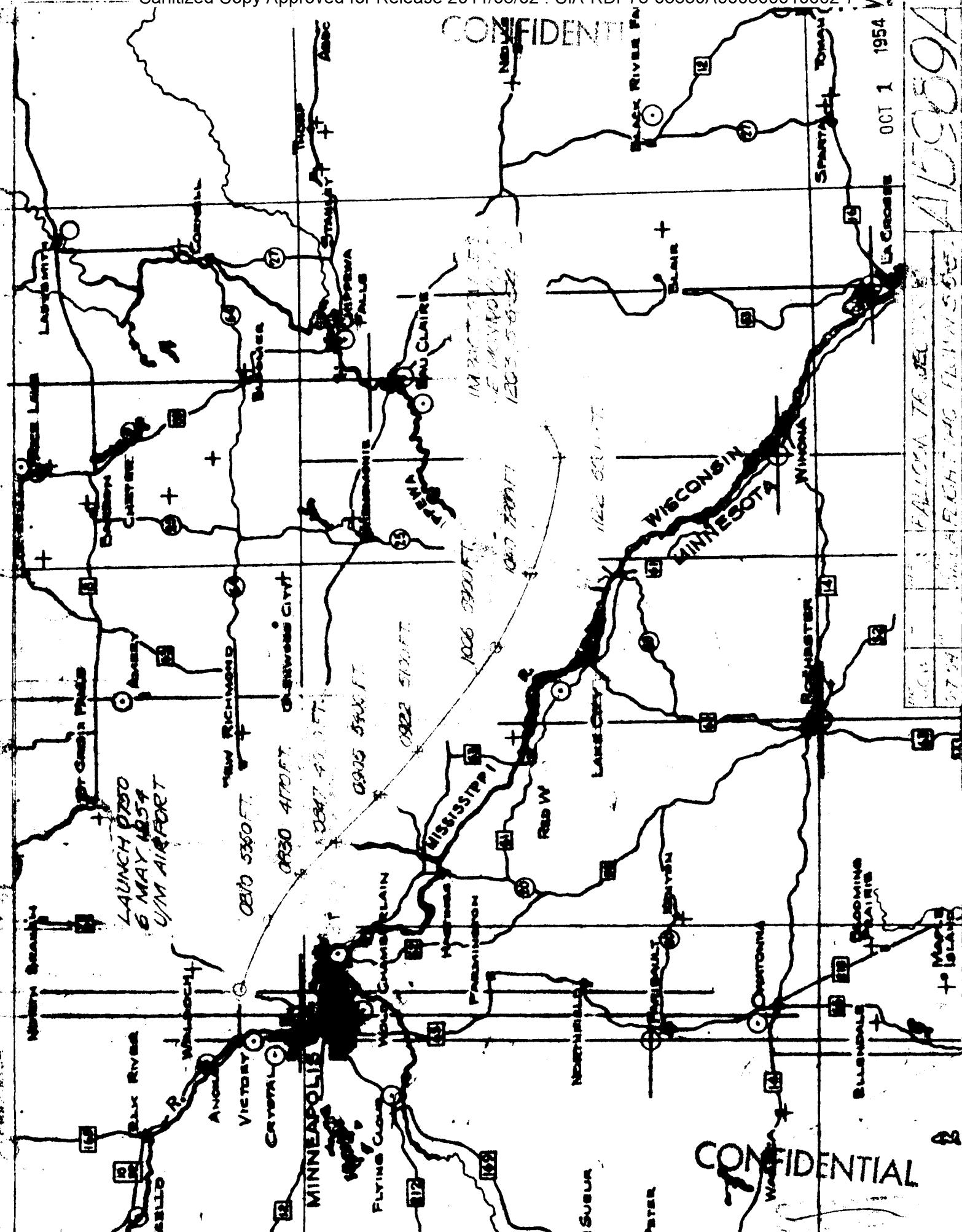
3724

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LOAD VS ALTITUDE
FOR 2635
VOLUME 8000 FT.³

HYDROGEN

HELIUM

GROSS LOAD IN POUNDS

532

532

532

532

532

532

532

532

OCT 1 1954

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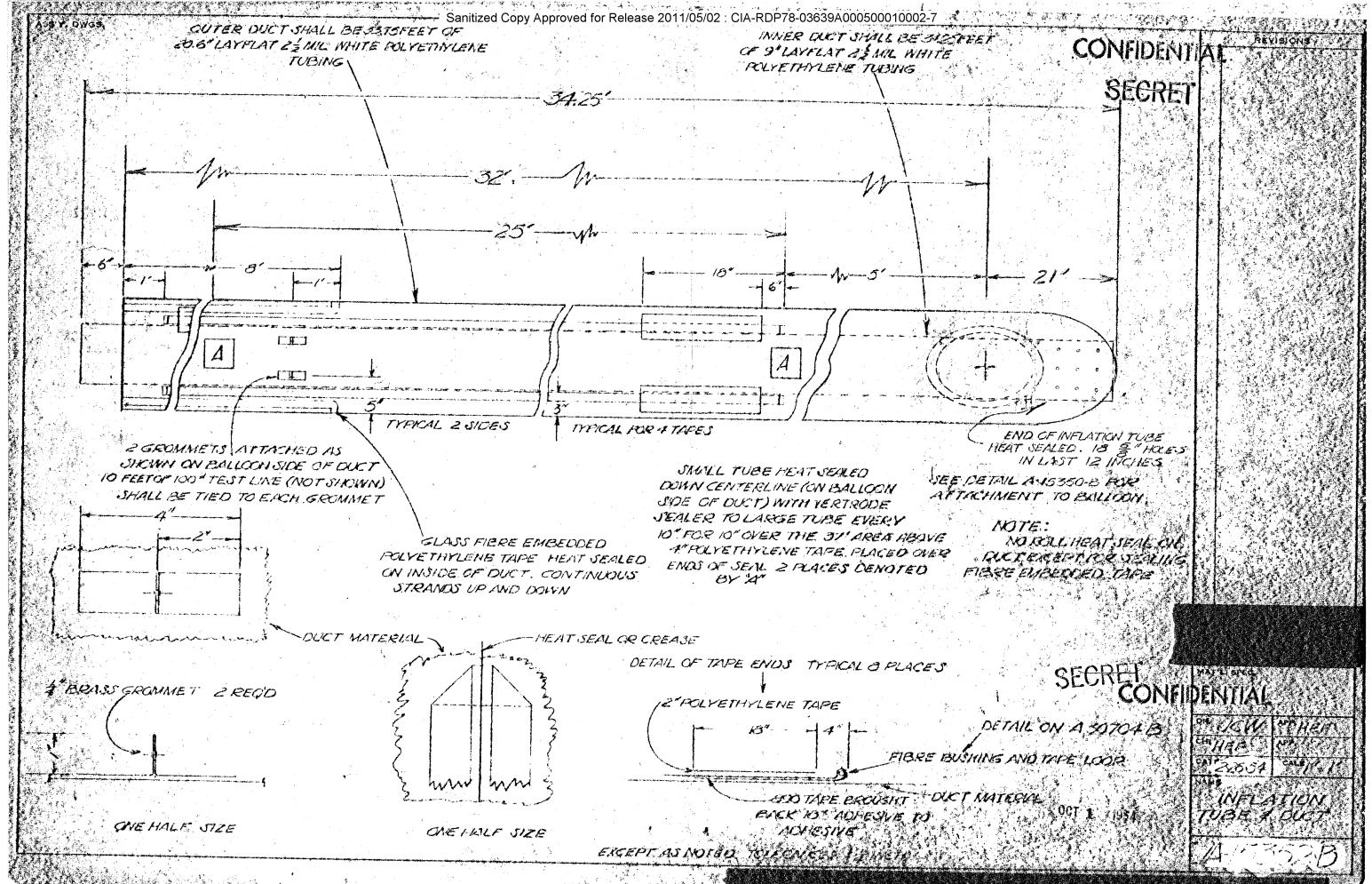
263P DRAWINGS

A-15352-B	Inflation Tube and Duct
A-15351-B	Duct Installation
A-15394-B	Reefing Sleeve
A-15350-B	Duct Attachment
A-16596-B	Gore Pattern
A-16749-B	Location of Wedge Core Tapes
A-16621-C	Valve and Rip Panel Installation
A-17232-C	263P Assembly
A-30004-A	Rip Panel Bolt
A-30005-A	Rip Panel Nut
A-30006-A	Rip Panel Gasket
A-11877-A	Suspension Harness
A-30704-B	Fibre Bushing Installation
A-11876-B	Attachment Pad
A-30708-B	Balloon Base
A-12072-B	Seal thru Balloon Base
A-16883-A	One Way Clip
A-16619-B	Device for Securing Duct
A-16618-C	Rip Device for Balloon Base

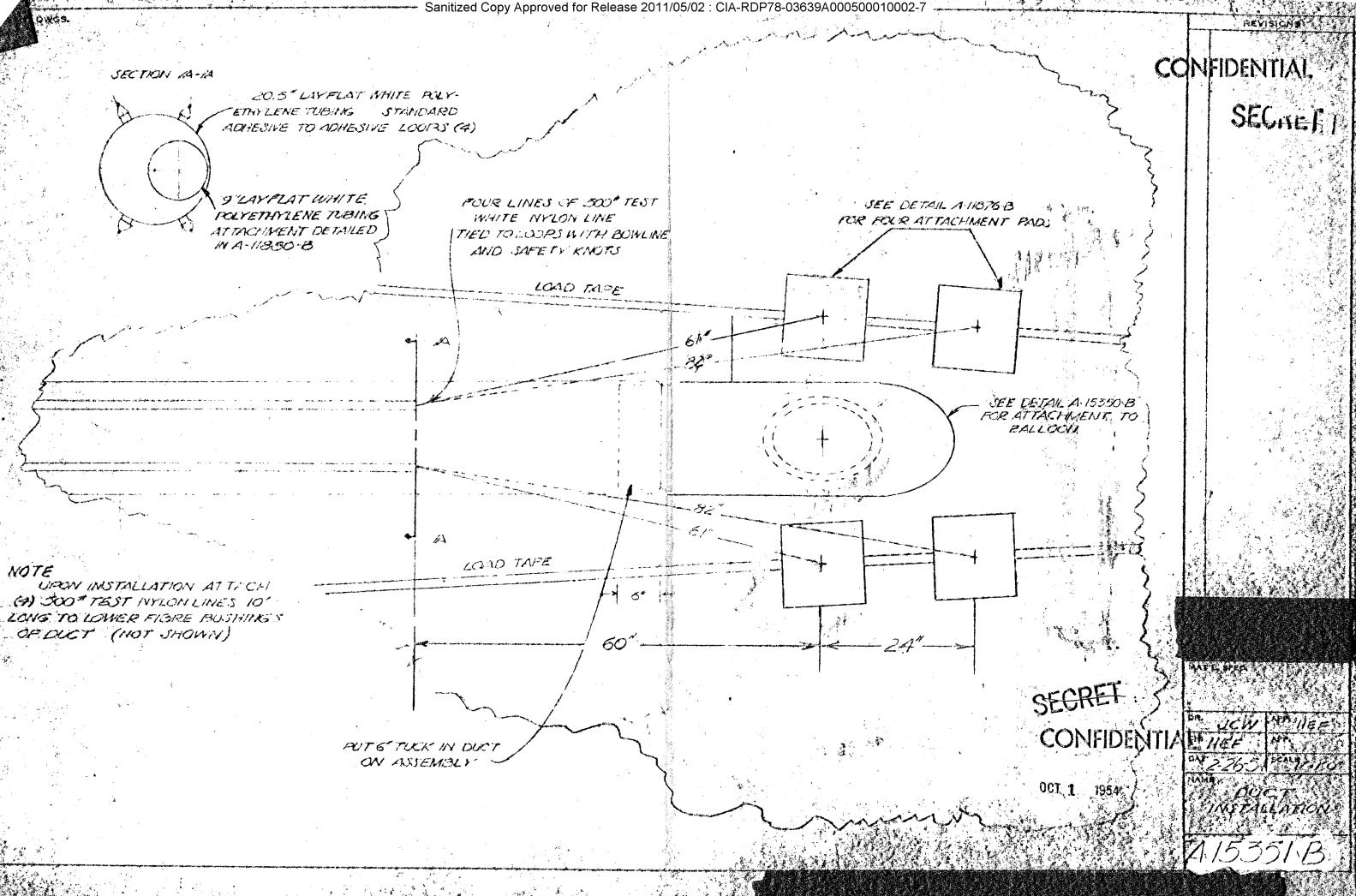
Valve Drawings

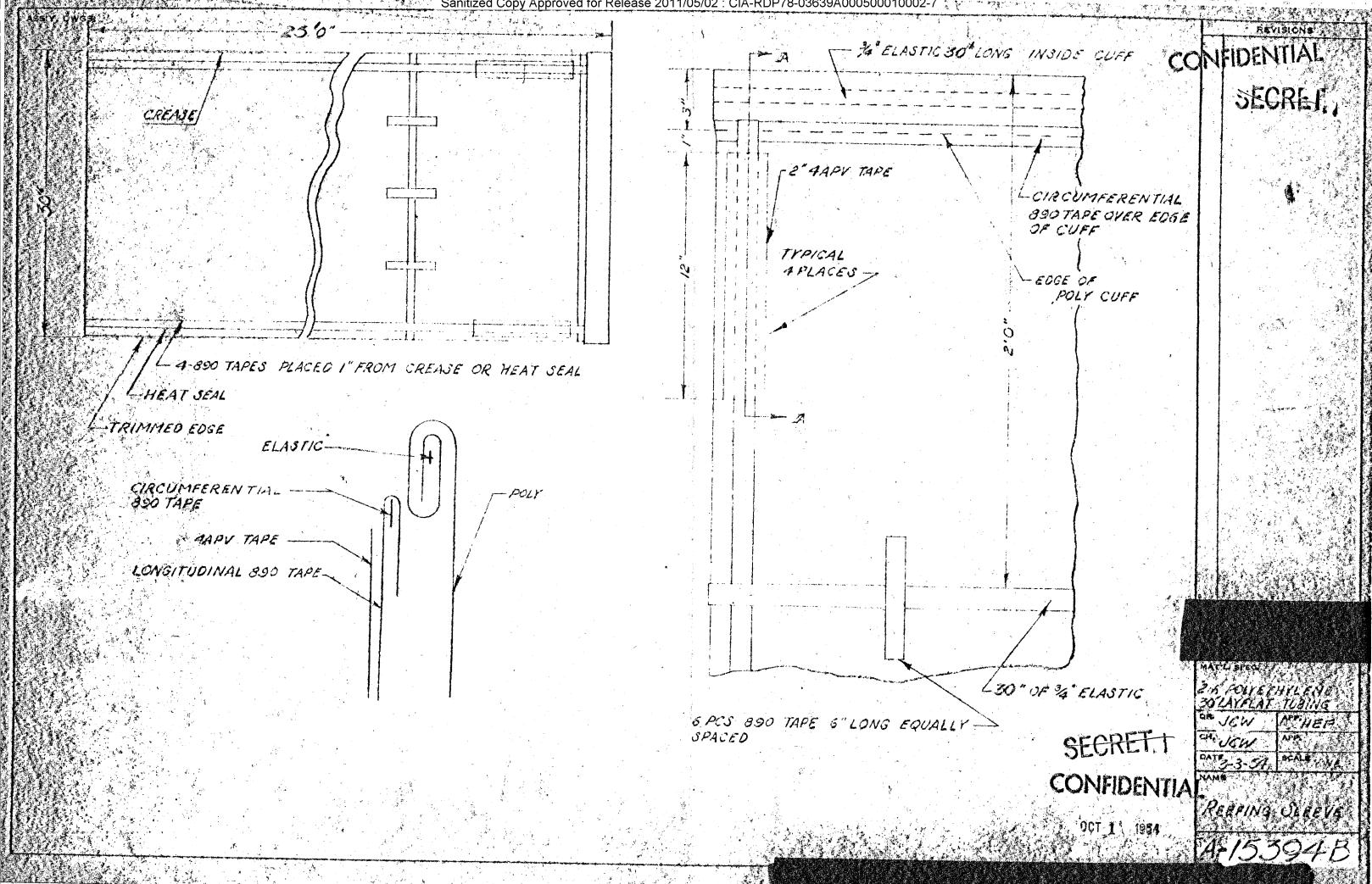
A-16525-A	Valve Spring
A-16524-A	Stud
A-16523-B	V Seat Mtg. Disk
A-16553-B	Valve Seat
A-16521-C	Valve Plate
A-16554-C	Valve Screen
A-16552-C	Valve Gasket
A-16551-C	Valve Ring
A-16555-C	Valve Assembly

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HEAT SEAL DUCT TO BALLOON
WITH 5 $\frac{1}{2}$ " LONG VERTRODE
SEAL SEGMENTS ON THIS
CIRCUMFERENCE. NO VOIDS IN
THE SEAL CAN BE TOLERATED.

HEAT SEAL 3" WIDE
GLASS FIBRE EMBEDDED
POLYETHYLENE FILAMENT
TAPE TO THE BALLOON IN THIS AREA
WITH ROLL HEAT SEALER

OPENING IN BALLOON AND DUCT

NOTE

HOLE TO BE LOCATED 12 FEET FROM
TOP OF BALLOON MIDWAY BETWEEN
LOAD TAPES ON GORE AS SHOWN ON
DRAWING NO. 1A

1" WIDE BY 2" LONG
POLYETHYLENE TAPE
OVER HEAT SEAL OF
DUCT TO BALLOON

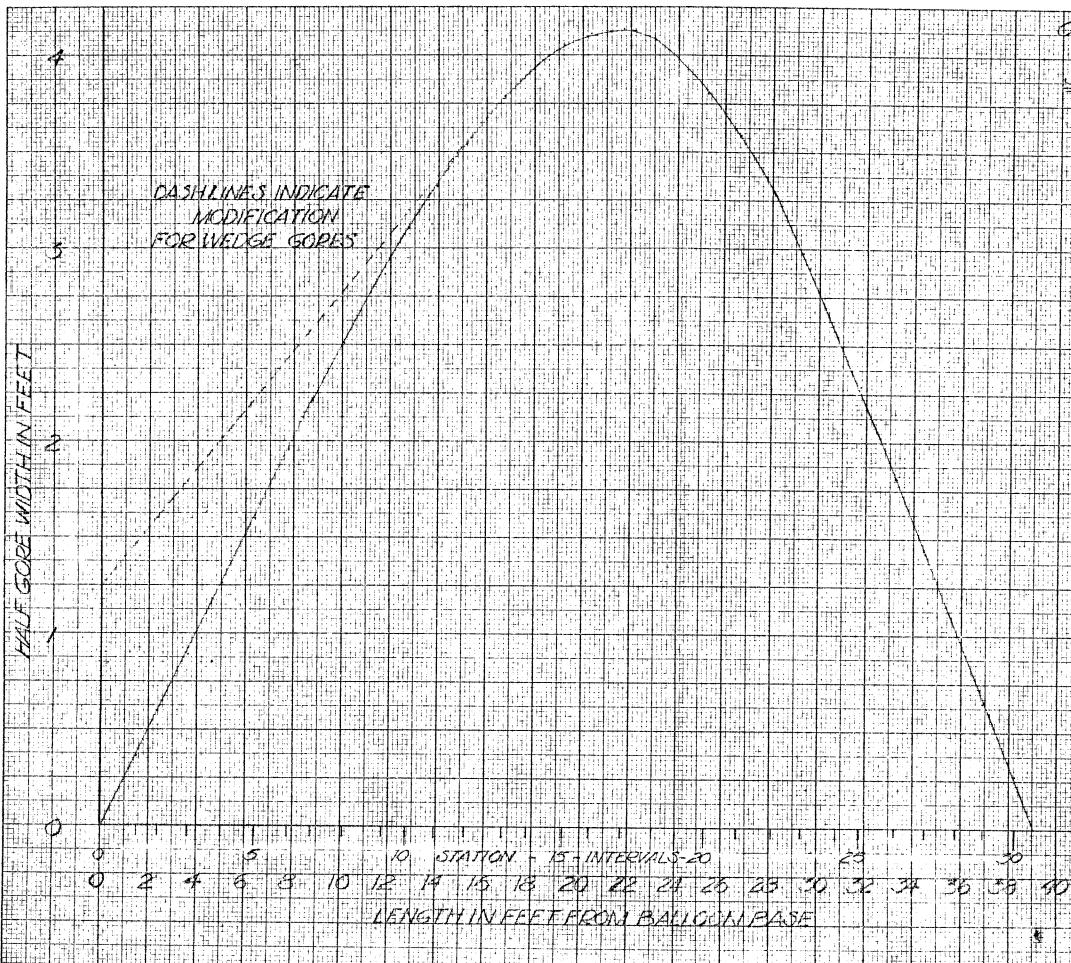
EXCEPT AS NOTED ALL
TOLERANCES $\pm .1$ EACH

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CORE PATTERN FOR 263P WITH WEDGE CORE		
STATION	DIST. IN FEET	SEG. W. IN FT.
1	1.43547	0.3665
2	2.40244	0.6016
3	3.6274	0.9054
4	5.0237	1.2672
5	6.3233	1.5977
6	7.6073	1.9016
7	8.8866	2.2145
8	10.0269	2.5231
9	11.1117	2.8150
10	12.3310	3.1026
11	13.5925	3.3726
12	13.0391	3.5324
13	10.2385	3.7221
14	17.8152	3.9127
15	12.3309	4.0616
16	20.3302	4.1135
17	21.6240	4.1351
18	23.0245	4.0337
19	24.0391	3.9023
20	25.3451	3.8117
21	26.6721	3.5075
22	23.0373	3.2010
23	22.3339	2.9219
24	30.3412	2.5497
25	31.18524	2.2550
26	35.26511	1.8047
27	34.46423	1.4212
28	35.14455	1.0047
29	36.92562	0.6592
30	37.47300	0.2503
31	39.00000	0

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A-15596-B

B-1-32

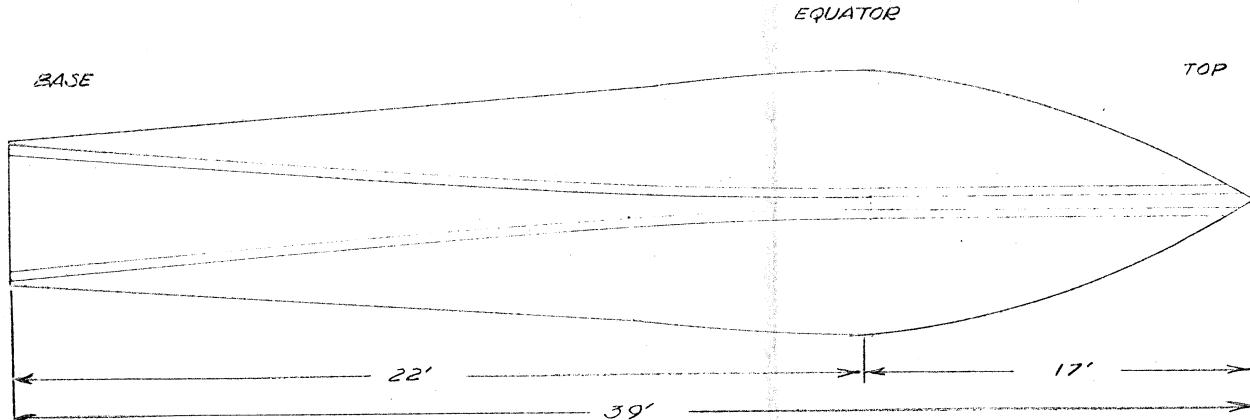
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A53Y. DWGS.

REVISIONS

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TWO 890 LOAD TAPES TAPER TOWARDS
CENTER OF WEDGE GORE AT THE BALLOON
EQUATOR THEN STRAIGHT TO TOP OF BALLOON

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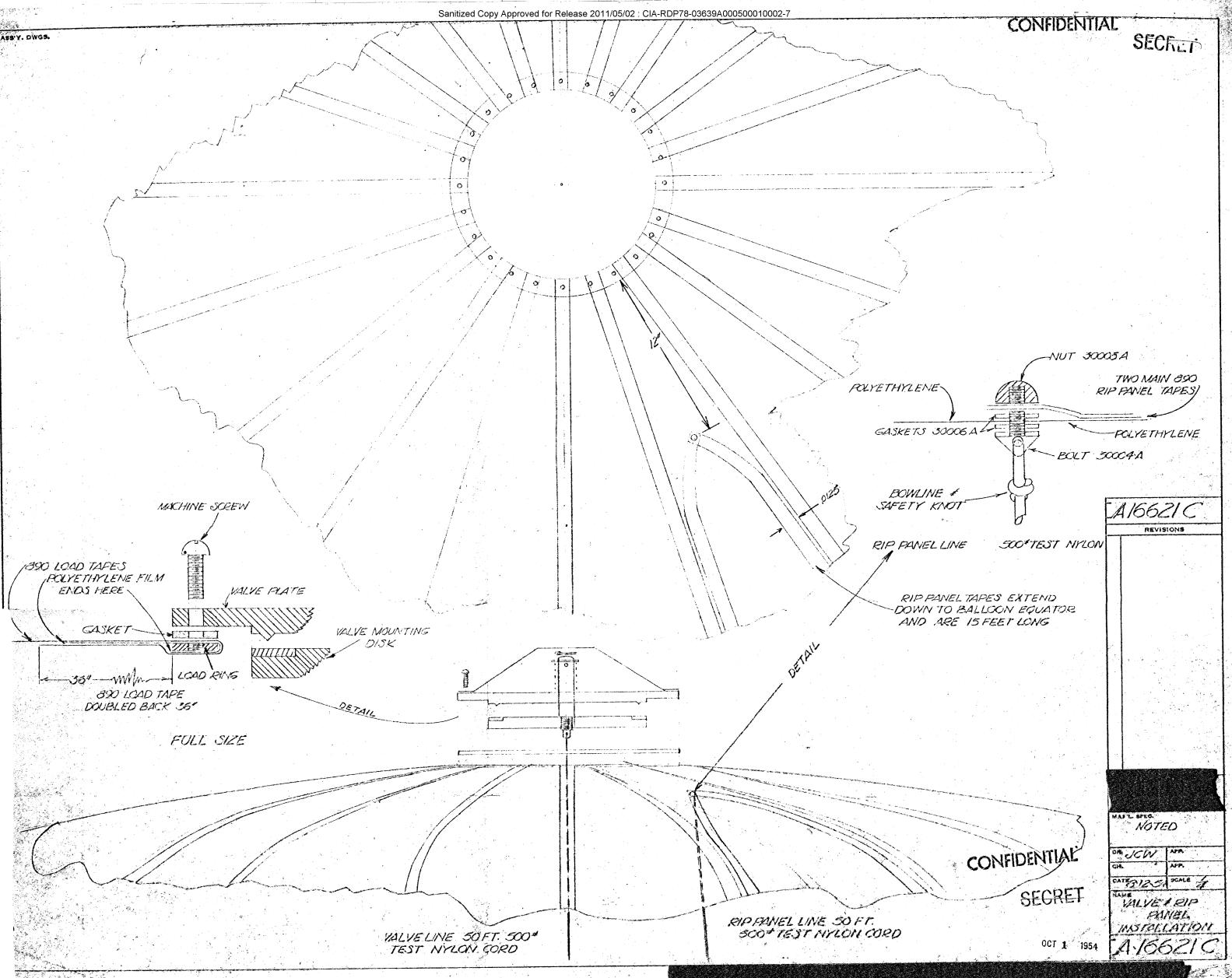
MAT'L. SPEC.	
DR. JCW	APP.
CH.	APP.
DATE 3/954	SCALE 1/36
NAME	
LOCATION OF WEDGE GORE TAPE	
A16749 B	

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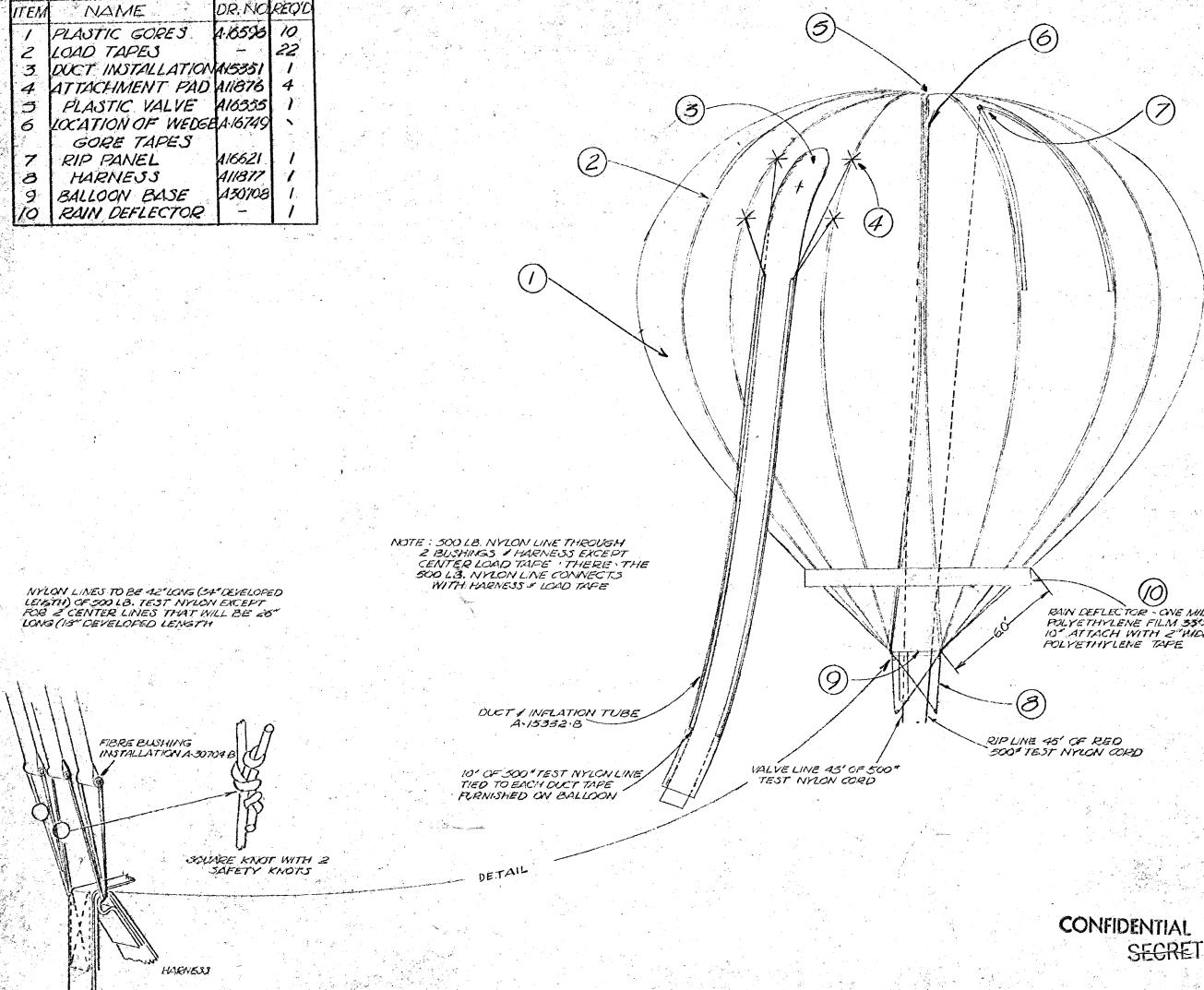
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ABY-DWGS.

LIST OF COMPONENTS		
ITEM	NAME	DR. NO. REQ'D
1	PLASTIC GORES	A-16538 10
2	LOAD TAPES	- 22
3	DUCT INSTALLATION	A15331 1
4	ATTACHMENT PAD	A11876 4
5	PLASTIC VALVE	A16335 1
6	LOCATION OF WEDGE	A-16749
	GORE TAPES	
7	RIP PANEL	A16621 1
8	HARNESS	A11877 1
9	BALLOON BASE	A30708 1
10	RAIN DEFLECTOR	- 1



A-17232C

REVISIONS

EXCEPT AS NOTED ALL PARTS ARE DRAWN GENERAL MILLS MECH. DIV. ENGINEERING RESEARCH & MANUFACTURING SPECIFICATIONS APPL MATERIALS AND METHODS
NOTED

DR. UCW APP
CH- APP
DATA 30-5A SCALE 1-3'
NAME
263P ASSEMBLY

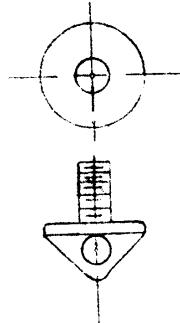
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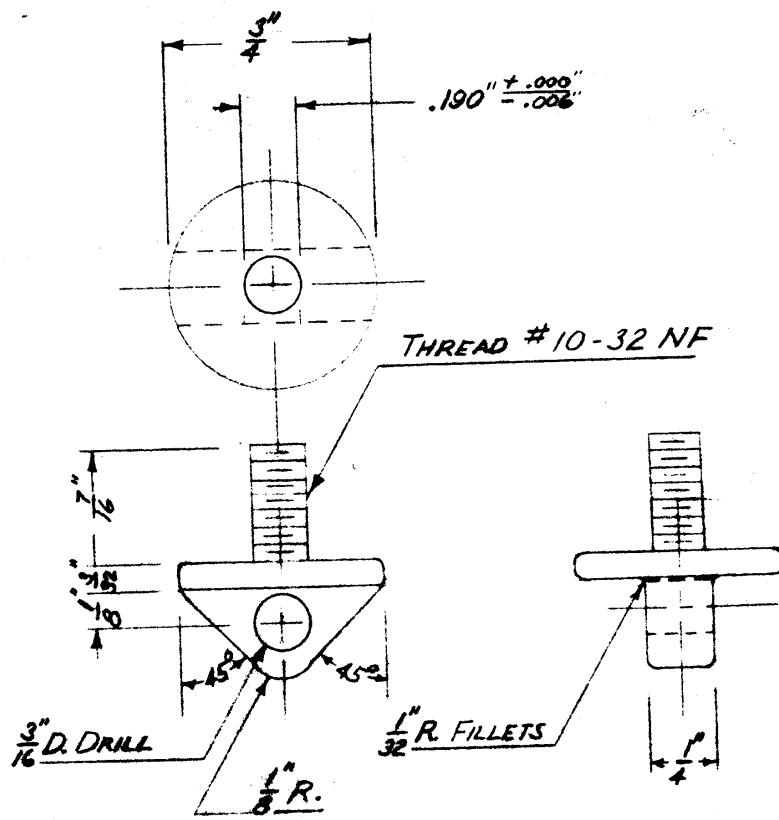
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ACTUAL SIZE

POLISH FINISH
ROUND ALL EDGES

卷之三



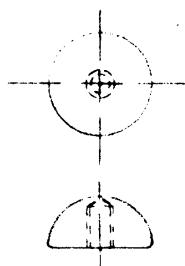
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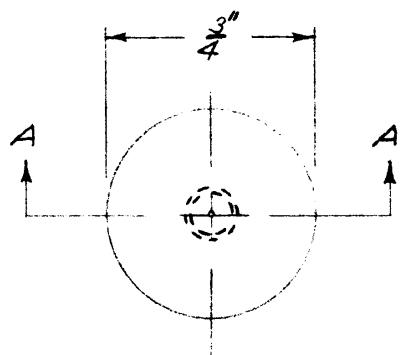
IF NOT SPECIFIED TOLERANCES ARE:
±.001" IF 3 DECIMAL FIGURES ARE GIVEN
±.01" IF 2 DECIMAL FIGURES ARE GIVEN
±.1" IF 1 DECIMAL FIGURE IS GIVEN

DR.	DICK	APP. F.C.	SCALE Double	MAT. ALUMINUM	NO. BOLTS ONE	NAME RIP PANEL CARD ATTACHMENT BOLT	A-30004-A
CAL.		APP. HEF	DATE 9-27-51	MAT. SPEC. 24ST	J-17A		

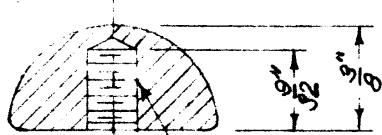
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ACTUAL SIZE



POLISH FINISH
ROUND ALL EDGES



DRILL #21 (.159) AS SHOWN
BOTTOM TAP #10-32 NF

SECRET

SECTION A-A

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IF NOT SPECIFIED TOLERANCES ARE:
±.005" IF 3 DECIMAL FIGURES ARE GIVEN
±.01" IF 2 DECIMAL FIGURES ARE GIVEN
±.1" IF 1 DECIMAL FIGURE IS GIVEN

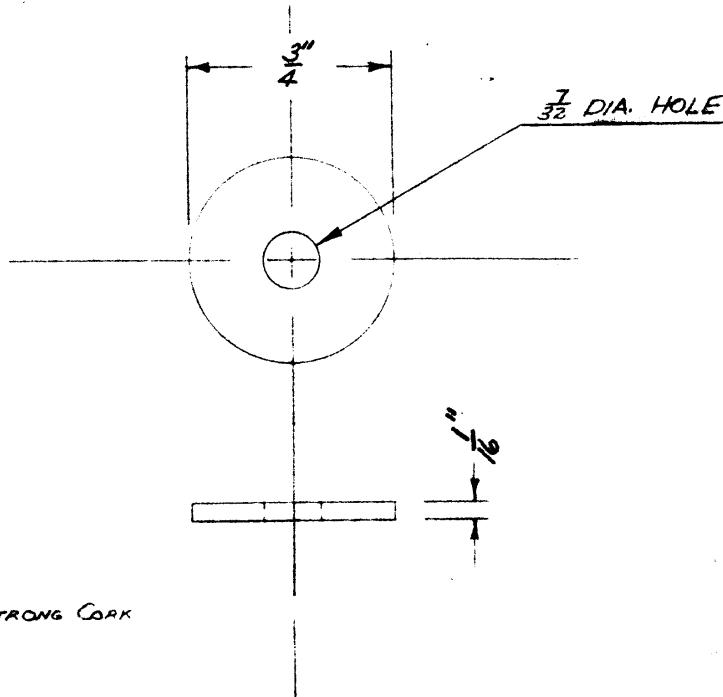
DR. DICK	APP. A	SCALE DOUBLE	MAT. ALUMINUM	NO. PRO'D. ONE	NAME RIO PANEL CORO	A-30005-A
CH.	APP. HEF	DATE 9-27-51	MAT. SPEC. 24 ST	J-171	ATTACHMENT NUT	

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ACTUAL SIZE

MATERIAL: NC-710 ARMSTRONG CORK
 $\frac{1}{6}$ " THICK

George



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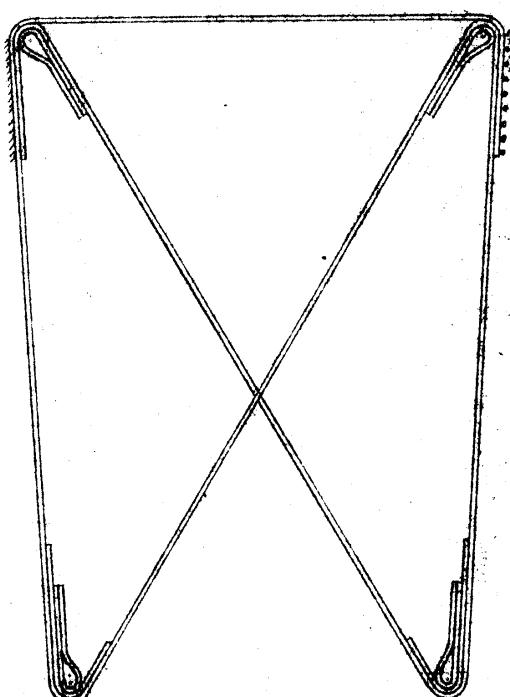
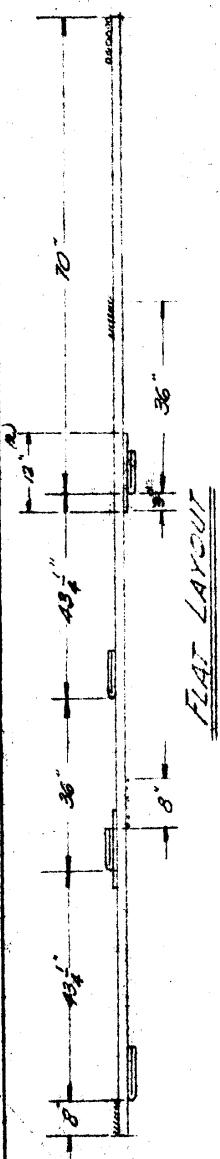
OCT 1 1954

IF NOT SPECIFIED TOLERANCES ARE:
±.001° IF 3 DECIMAL FIGURES ARE GIVEN
±.01° IF 2 DECIMAL FIGURES ARE GIVEN
±.1° IF 1 DECIMAL FIGURE IS GIVEN

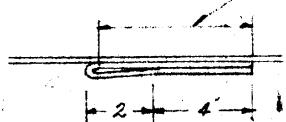
DR. DICK	APP. F	SCALE DOUBLE	MAT. CORK	NO. PEGS TWO	NAME RED PARROT CORD ATTACHMENT GASKET	A-30006-A
CH.	APP. HEC	DATE 9-27-51	MAT. SPEC. AC-710	J-174		

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NOTE: MATERIAL SHALL BE 1500 LB.
TEST (OR BETTER), 1 $\frac{1}{2}$ " WOVEN
WEBBING. 10' REQUIRED



SEW THIS PORTION OF STRAP FIRST
& THEN MAKE LOOP (USING
NO. 6 COTTON CORD)



SEW THIS PATTERN WITH
NO. 6 COTTON CORD

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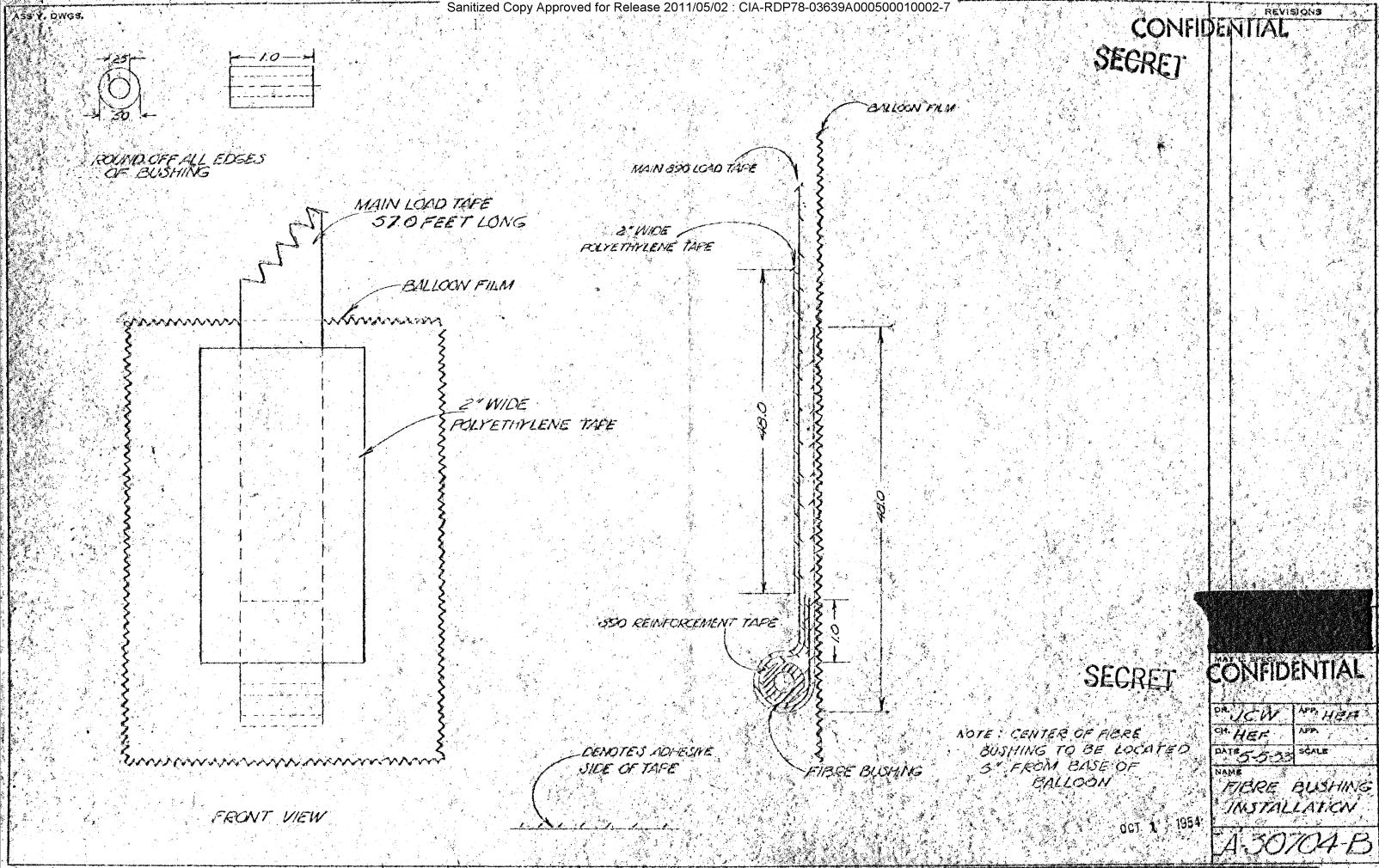
DETAIL OF EYE ATTACHMENTS

OCT 1 1954

RE: GJ	DATE: 10-26-53
APP: HEF	NAME: 302P SUSPENSION HARNESS

A-11877-A

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ADHESIVE TO ADHESIVE LOOK IN
TAPE #8 AND ON 12" HIGH

NOTE: TAPE 9-10-11-12 ARE TO TOUCH TAPE
NO. 7 & MUST FORM A 45° ANGLE
WITH TAPE NO. 3

ALL TAPE TO BE NO. 890 GLASS
FIGURE 1" WIDE TAPE EXCEPT
AS NOTED

POLY TAPE (1 $\frac{1}{2}$)

POLY TAPE (8")

102" POLY TAPE

2" CLOTH TAPE (TOTAL)

4" POLY TAPE, 1 $\frac{1}{2}$ " LONG (8")

4" POLY TAPE, 1 $\frac{1}{2}$ " LONG (8")

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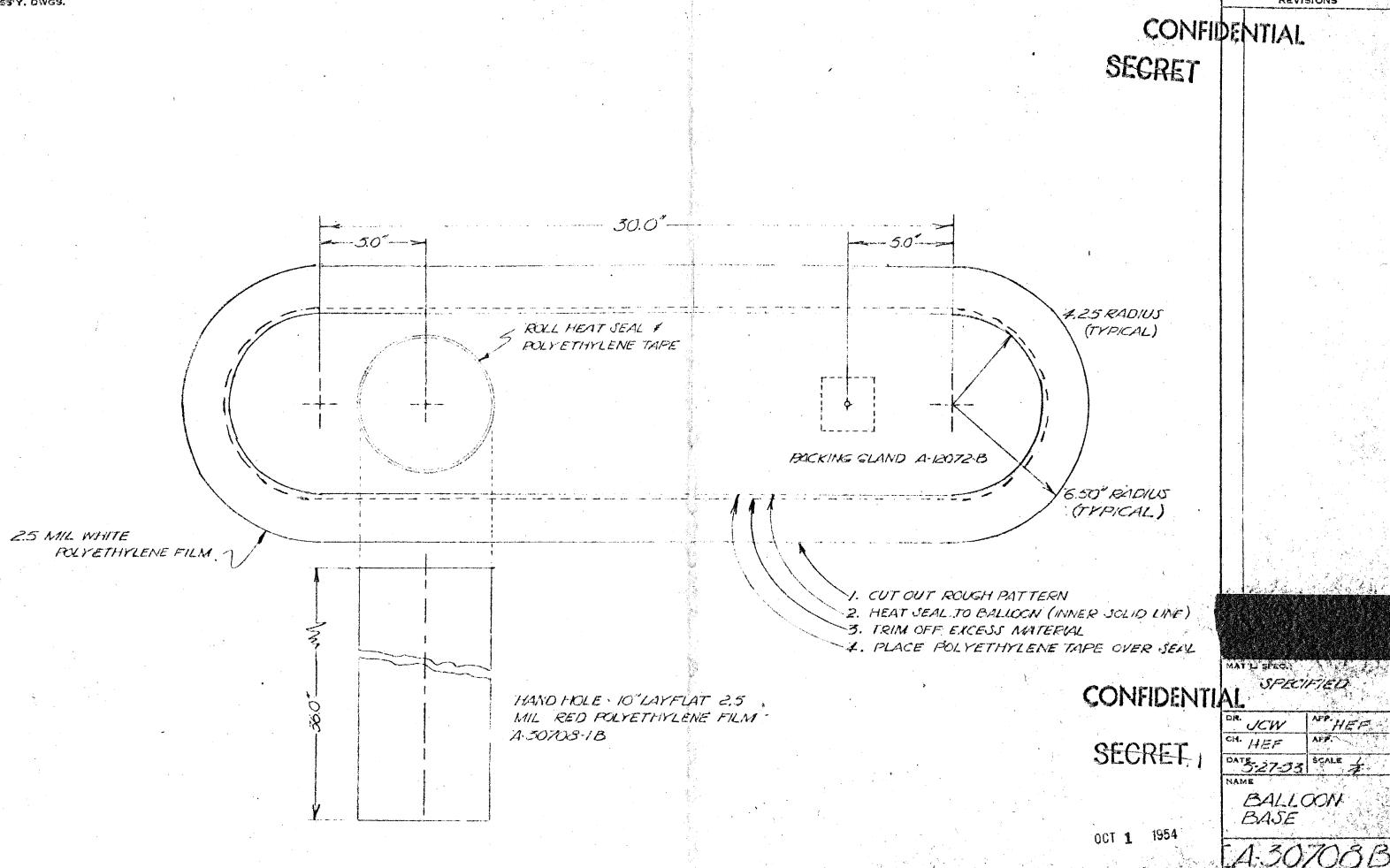
CB-TECHNICS
APP-11EF

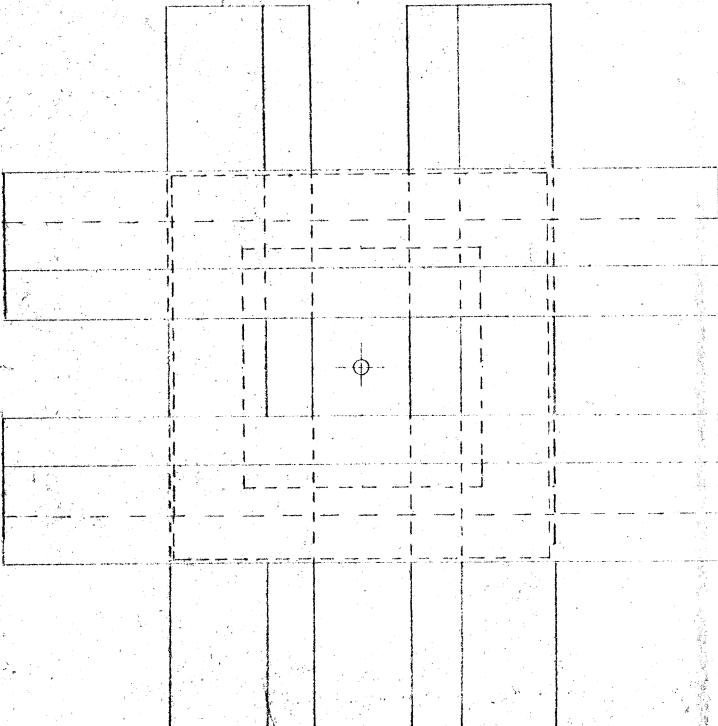
ATTACHMENT PAD

A-14376

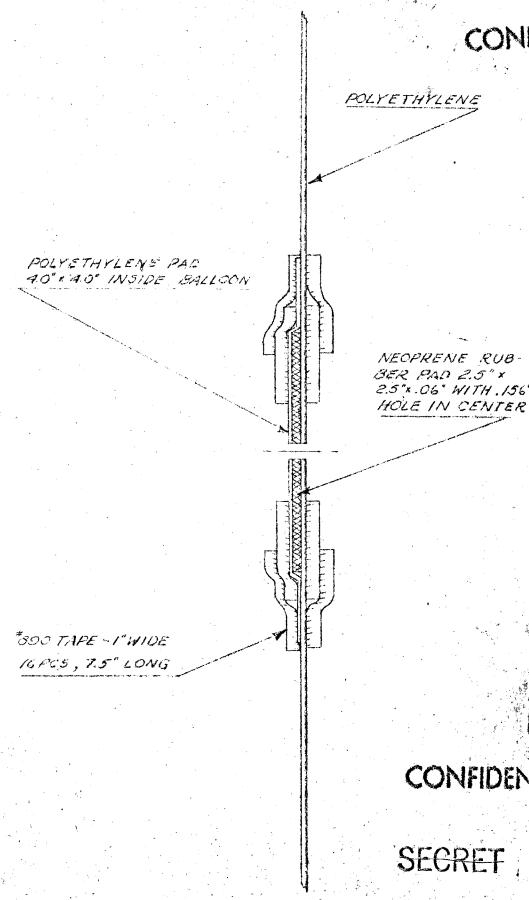
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ASY. DWGS.





NOTE: A SMALL HOLE SHOULD BE PIERCED THRU POLY MATERIAL IN LINE WITH HOLE IN NEOPRENE PAD BEFORE CORD (500 POUND TEST RED NYLON LINE) IS INSERTED.



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OCT 1 1951

NAME
SEAL THRU BAL-
LOON ENVELOPE

A-12072-B

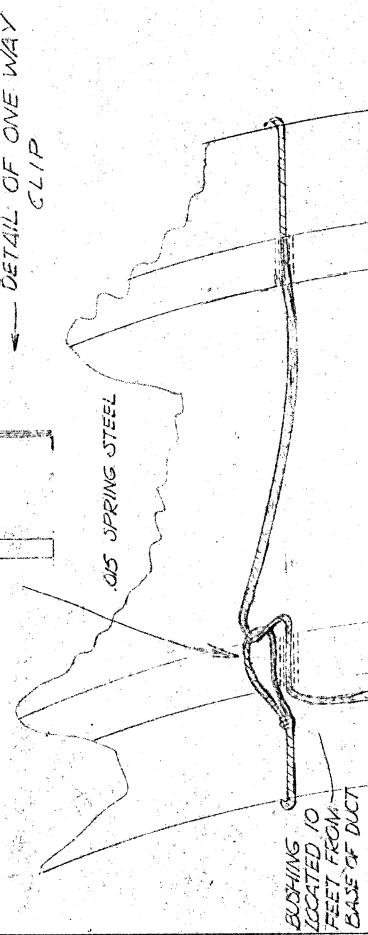
DR.	APP.
J.P.D	H.E.F
CH.	APP.
DATE	SCALE
3-9-53	FULL
NAME	
SEAL THRU BAL-	
LOON ENVELOPE	
A-12072-B	

1A16883A

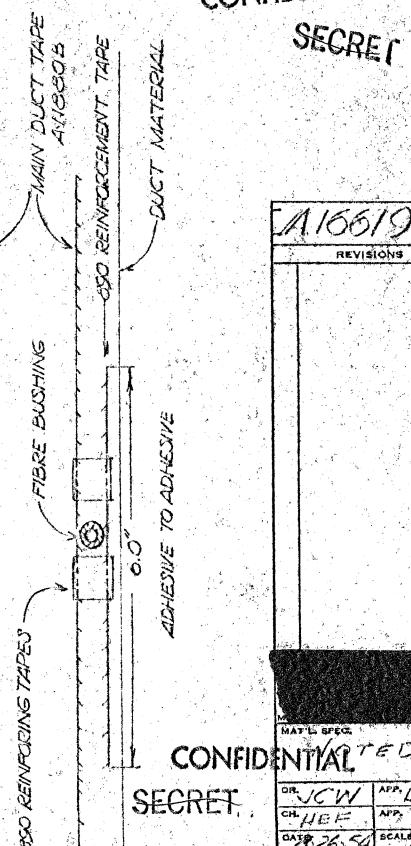
ASS'Y. DWGS	REVISIONS												
	<p>CONFIDENTIAL SECRET</p> <p>015 SPRING STEEL</p> <table border="1"><tr><td>DR.</td><td>CW</td><td>APP.</td></tr><tr><td>CH.</td><td></td><td>APP.</td></tr><tr><td>DATE</td><td>10-31-54</td><td>SCALE</td></tr><tr><td>NAME</td><td colspan="2">NONE</td></tr></table> <p>OCT 1 1954</p> <p>MURKIN</p>	DR.	CW	APP.	CH.		APP.	DATE	10-31-54	SCALE	NAME	NONE	
DR.	CW	APP.											
CH.		APP.											
DATE	10-31-54	SCALE											
NAME	NONE												

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FULL SIZE
ASSY DWGS.



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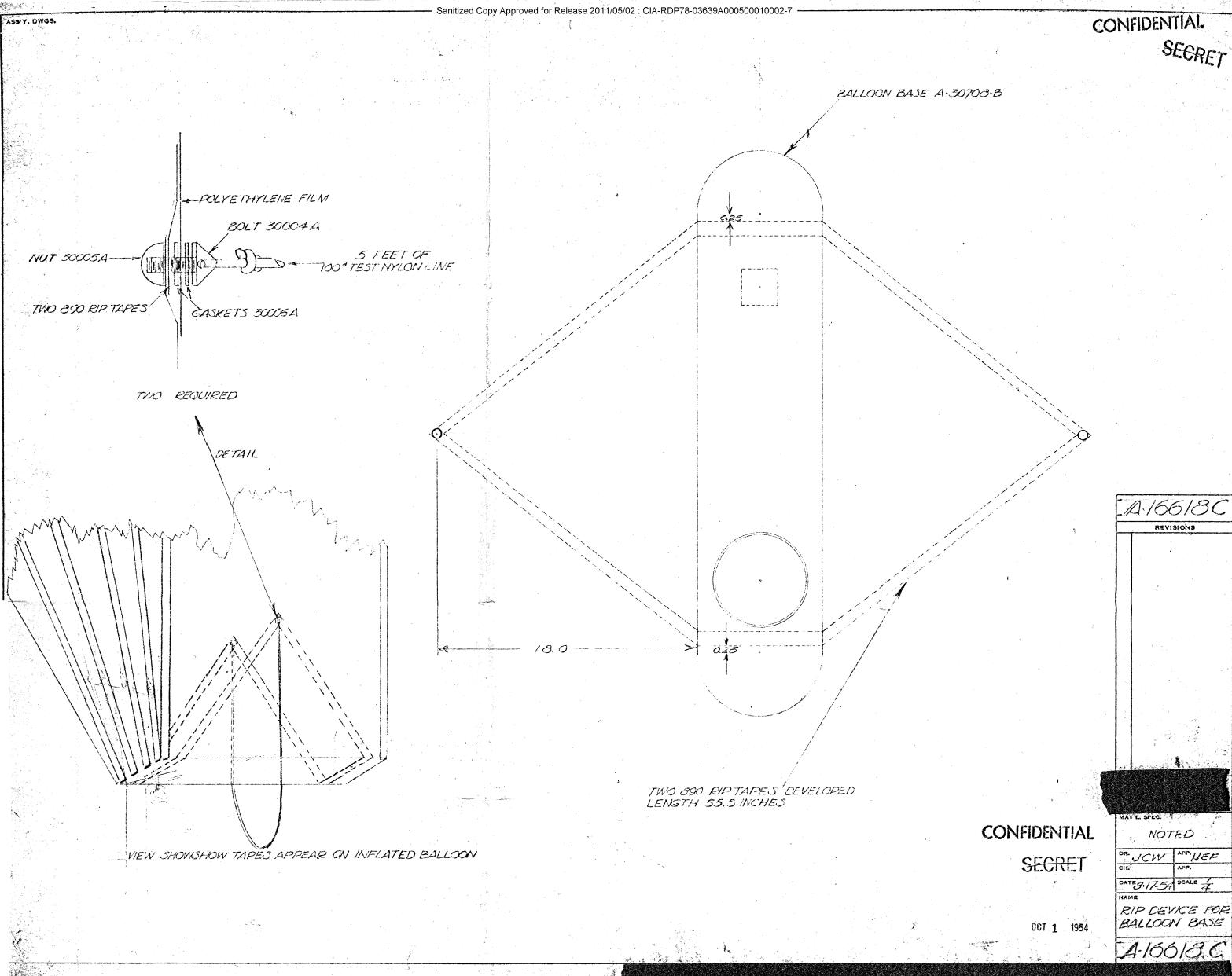
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SECRET

A16619-B
REVISIONS

MATERIAL SPEC.	
DR. JCW	APP. UEF
CH. HEE	APP
DATE 8-26-54	SCALE NONE
NAME	
DEVICE FOR SECURING DUCT	
OCT. 1 1954	
A16619-B	

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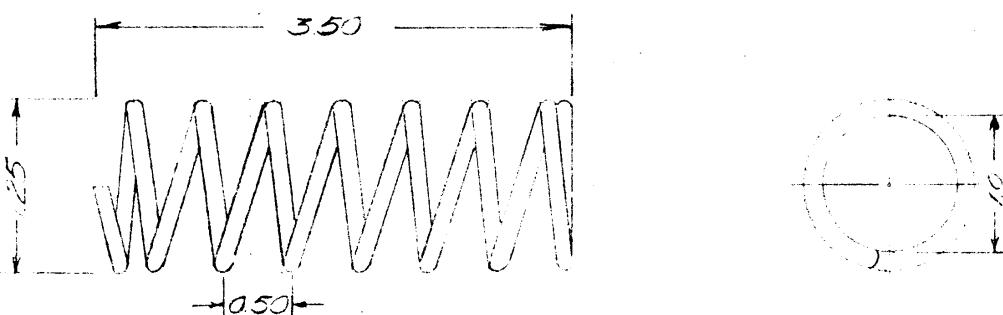


A-16525 A

ASS'Y. DWGS.

REVISIONS

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SPRING DATA

WIRE DIAMETER .125
SPRING CONSTANT 30 LBS INCH
NO. OF ACTIVE COILS 17
ENDS GROUNDED SQUARED

MATL SPEC
CADMIUM
PLATED WIRE

DR. JCW	APP. HEF
CH. HEF	APP.
DATE 8-25-54	SCALE FULL
NAME MS PLV SOC 16	

OCT 1 1954

A-16525 A

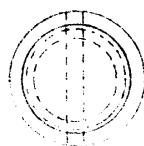
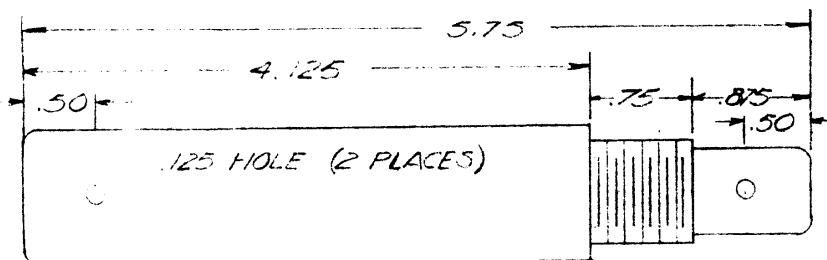
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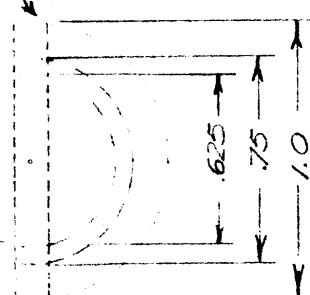
A16524 A

REVISIONS

ASS'Y. DWGS.



DETAIL



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MAT'L. SPEC.	
1" LINEN MICA VTA ROD	APP. HEF
DR. JCW	APP. HEF
CH. HEF	APP.
DATE 8-2-54	
SCALE FULL	
NAME	
STUD FOR M3 VALVE	

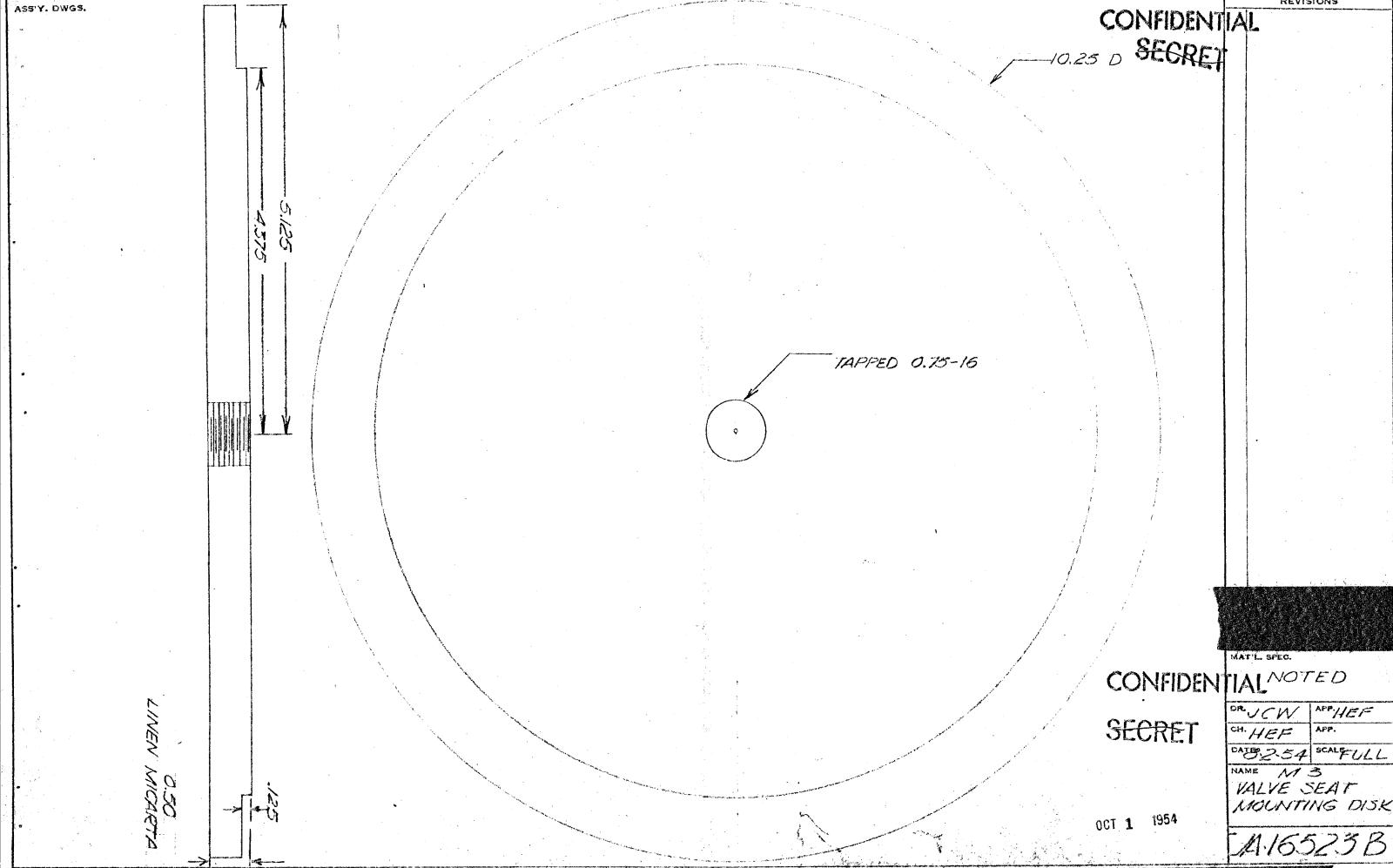
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SECRET

DOUBLE SIZE

OCT 1 1954

A16524 A



ASS'Y. DWG3.

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REVISIONS

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SECRET

5/25R
4/35R

.125 THICK 800
CLOSED CELL NEO.

DR.	JCW	APP.
CH.		APP.
DATE	8/1/54	SCALE FULL
NAME	VALVE SEAT	

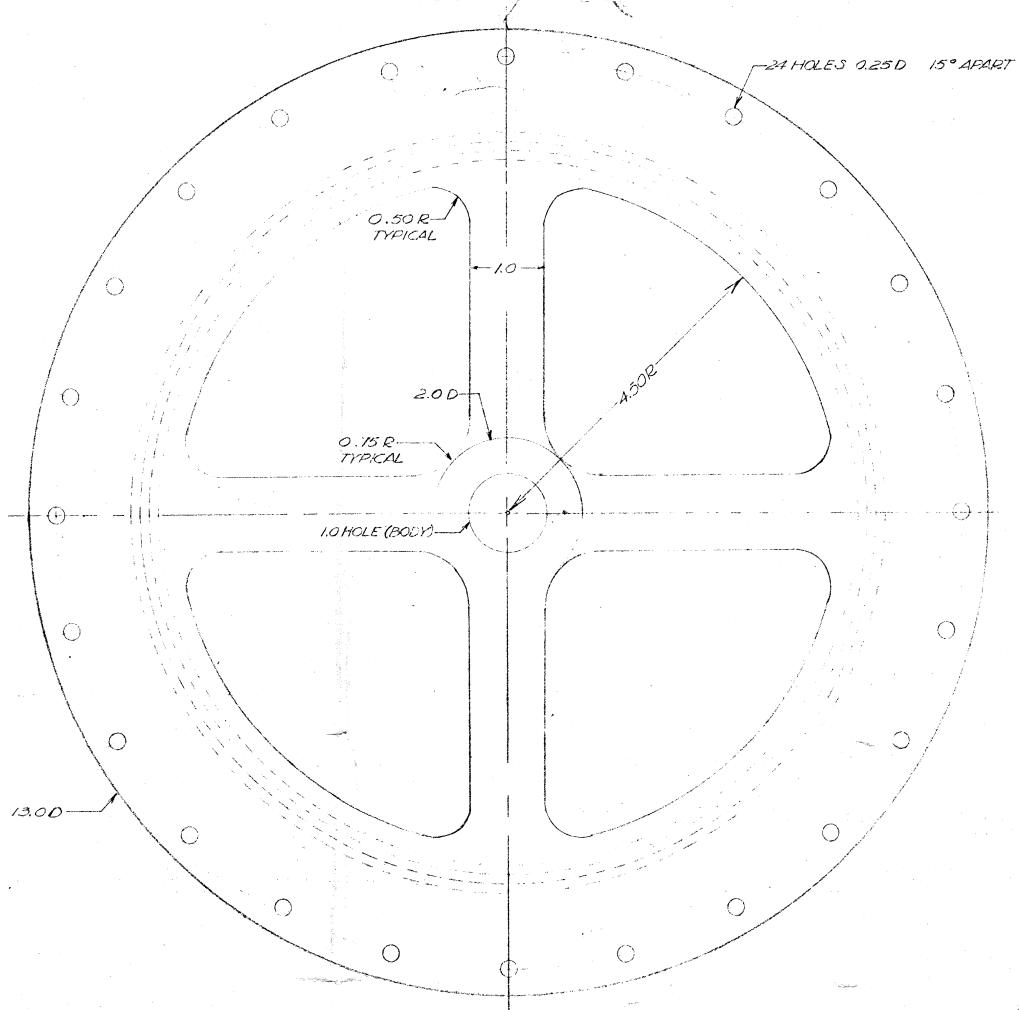
SECRET
CONFIDENTIAL

OCT 1 1954

116553B

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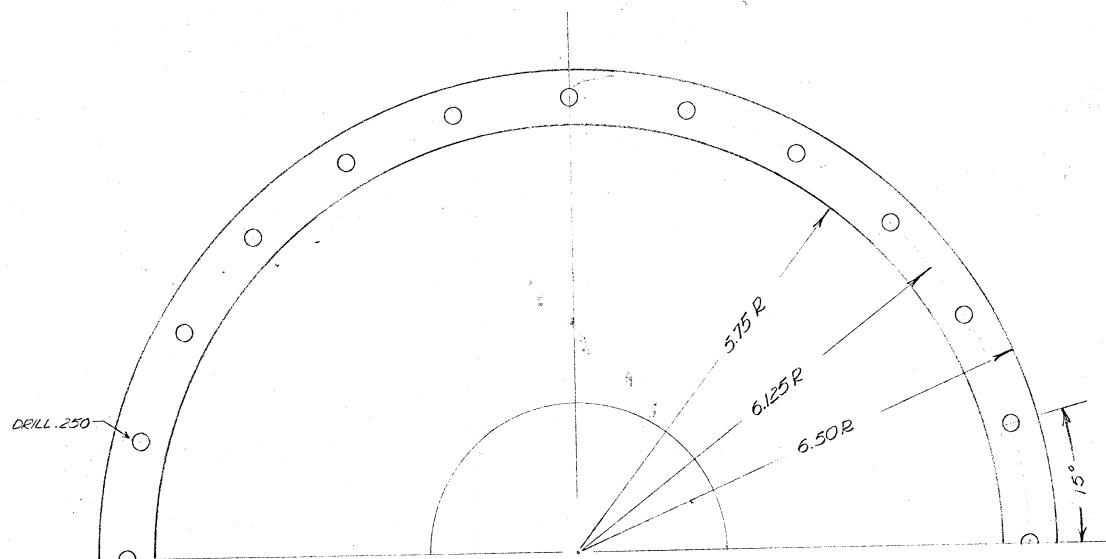


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MATE SPEC	
-5625 LINEN MICARTA	
DR.	JCW
CH	HEF
DATE	7305A
NAME	
M3 PLASTIC VALVE PLATE	
A16521C	

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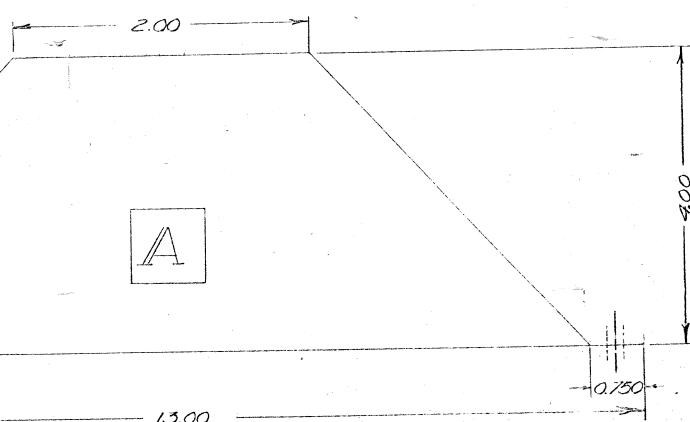
A



12x12 MESH
.018 WIRE DIAMETER
.065 OPENING

ENDS OF SCREEN
SOLDERED ALONG THIS
EDGE

.0375



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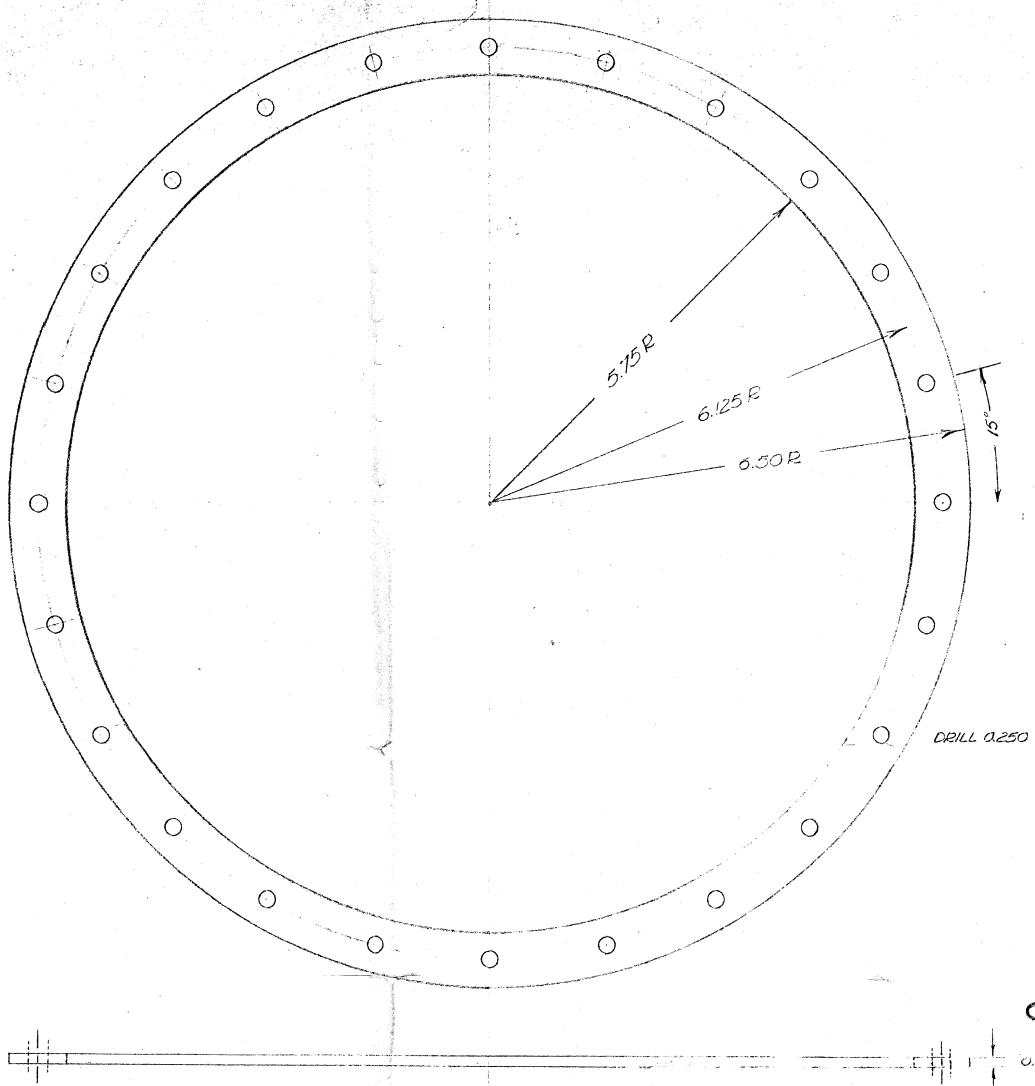
SECRET

A-16554C

DATE	1954
NAME	M-3 VALVE SCREEN
NOTE	FULL

OCT 1 1954

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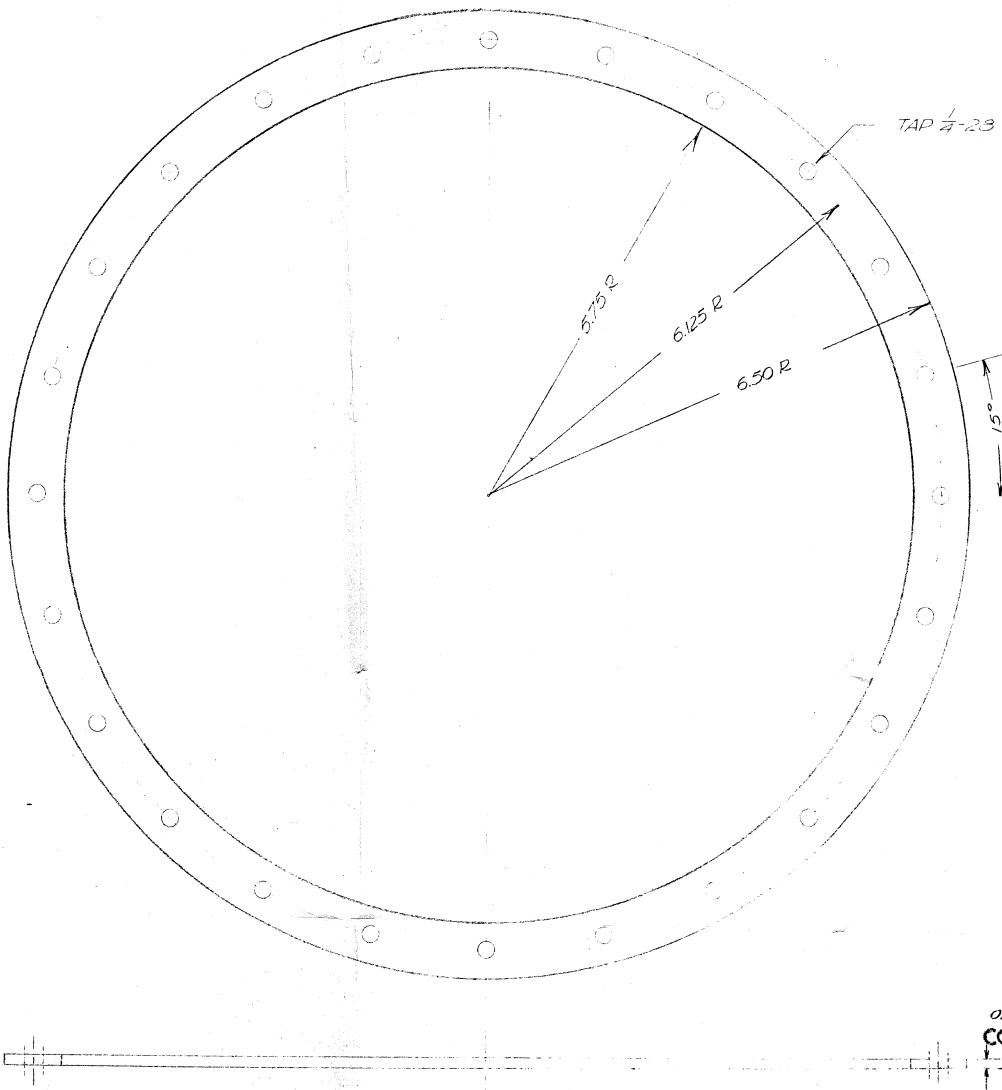
A16552 C
REVISIONS

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SECRET

MATERIAL: RUBBER
INTEGRATED CORK
DR. JCW APP.
CH. APP.
DATE 9-5-54 SCALE FULL
NAME VALVE
MOUNTING GASKET
OCT 1 1954
A16552 C

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SECRET



A16551 C

REVISIONS

MAPLE SPEC.
0.125 24-ST.
ALUMINUM

DR. JCW APR
CH. APR

DATE 9-3-54 SCALE FULL

NAME

VALVE
MOUNTING RING

0.125
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A16551 C

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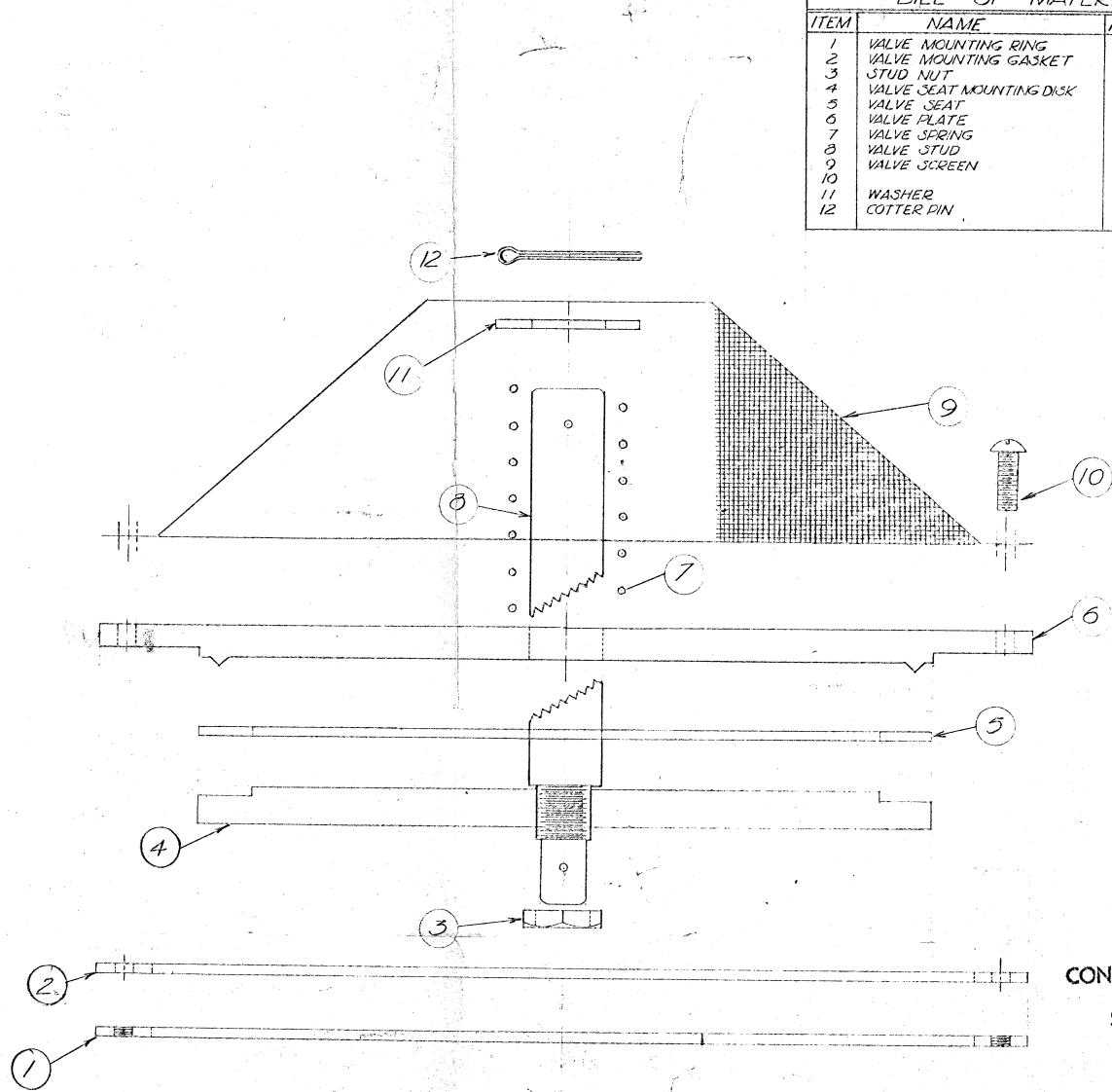
SECRET

ASSY. DWGS.

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BILL OF MATERIALS

ITEM	NAME	NO. REQ'D	DRAW. NO.
1	VALVE MOUNTING RING		A16531 C
2	VALVE MOUNTING GASKET		A16532 C
3	STUD NUT		
4	VALVE SEAT MOUNTING DISK		A16323 C
5	VALVE SEAT		A16533 B
6	VALVE PLATE		A16321 C
7	VALVE SPRING		A16525 A
8	VALVE STUD		A16524 A
9	VALVE SCREEN		A16554 C
10			
11			
12	WASHER COTTER PIN		



A16555 C

REVISIONS

MATERIAL SPEC. NOTED

DR. JCW	APM HEIC
CH HEP	APP.
DATE 9-54	SCALE 1:1
NAME: M-3 VALVE ASSEMBLY	
A16555 C	

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OCT 1 1954

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